



BEING **ENERGY**



DELIVERABLE

Project Acronym: BeingEnergy

Grant Agreement number: 303476

Project Title: Integrated low temperature methanol steam reforming and high temperature polymer electrolyte membrane fuel cell

D3.6 - CO₂ selective membranes

Revision: 1.0

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Project co-funded by the FCH-JU within the Seventh Framework Programme		
Dissemination Level		
P	Public	
C	Confidential, only for members of the consortium and the Commission Services	x

Revision History

Revision	Date	Author	Organisation	Description
1.0	01/09/2014	Adélio Mendes, Márcia Andrade, Marta Boaventura, Paulo Ribeirinha,	UPORTO	First version

Statement of originality:

This deliverable contains original unpublished work except where clearly indicated otherwise. Acknowledgement of previously published material and of the work of others has been made through appropriate citation, quotation or both.

TABLE OF CONTENTS

	Page
1. Executive Summary	5
2. Developed work	6
2.1 <i>Introduction</i>	<i>6</i>
2.2 <i>Experimental</i>	<i>6</i>
2.3 <i>Results and discussion</i>	<i>7</i>
3. Conclusions	9
Bibliography	10

TABLE OF FIGURES

Figure 1 CO₂ adsorption equilibrium isotherms for PIL1-40IL1 at 25 °C, 100 °C and 200 °C (lines were added for readability)..... 7

Figure 2 CO₂ adsorption equilibrium isotherms for PIL2-20IL2 at 25 °C (lines were added for readability)..... 7

1. Executive Summary

Task 3.4 of project BeingEnergy refers to the preparation and characterization of membranes and membrane modules for selective removal of CO₂. The goal was to produce and characterize polymer / ionic liquids membranes. Various ionic liquids were to be prepared and accessed. At M32 it was intended to report on high temperature CO₂ selective membranes (milestone MS05) concerning CO₂ permeability and the CO₂/H₂ selectivity.

This work characterizes four suitable polymeric ionic liquid-based membranes for low temperature methanol steam reforming (MSR) application, for CO₂ removal. Polymeric ionic liquids were prepared with 40 wt.% and 20 wt.% of free ionic liquid (samples PIL1-40IL1 and PIL2-20IL2) and without free ionic liquid (PIL1 and PIL2). PIL1-40IL1 and PIL2-20IL2 composite membranes present high CO₂ diffusivity and sorption and negligible H₂ diffusivity and sorption. For PIL1-40IL1 CO₂ permeance was higher than H₂ permeance. On the other hand, PIL1 and PIL2 present higher permeances for H₂ rather than for CO₂. Therefore, it can be presumed that free IL compounds may enhance the CO₂ permeance.

Taking into account the comments and recommendations of the Mid-Term Review of the project (FCH-JU 2014 D2612), task 3.4 (Preparation and characterization a membrane and membrane module for selective CO₂ removal) was reassessed. Considering the limited improvements regarding the development and characterization of CO₂ selective membranes and the complexity of the hybrid MSR reactor, no further efforts will be made regarding task 3.4.

2. Developed work

2.1 Introduction

Methanol steam reforming (MSR) is being used to supply high temperature polymer membrane fuel cells (HT-PEMFC). Methanol reforming is endothermic while HT-PEMFC produces heat; if the two devices are run at the same temperature, ca. 180 °C – 190 °C, energy integration becomes possible. Also, at lower reforming temperature less CO is produced and catalyst is more stable. At this low temperature MSR needs a significantly more active catalyst. Despite the recent efforts for developing such catalyst, the best result up to now is a catalyst ca. 2x more active than catalyst by BASF. Other approach is the selective removal of hydrogen or carbon dioxide from the reaction medium [1]. For high methanol conversions the backward reaction becomes relevant and removing hydrogen from the reaction medium stops the backward reaction increasing the overall effective reaction kinetics [2]. Though attractive, this strategy hides the high-energy consumption needed for driving hydrogen out of the reactor – using either a pump or water vapour sweep gas. For CO₂ removal, air can be used as sweep gas (ca. 400 ppm CO₂),. Despite palladium membranes work quite well for hydrogen removal there is no membrane for removing selectively CO₂ at MSR conditions [2]. Preliminary results show that supported polymeric ionic liquid-based membrane selective for CO₂ can work at 180 °C improving the reaction kinetics of the MSR and decreasing the production of CO. When the HT-PEMFC feed is changed from pure hydrogen to direct reformat feed, the stoichiometric hydrogen increases ca. 30 %. This work characterizes four suitable polymeric ionic liquid-based membrane for low temperature steam reforming.

2.2 Experimental

- Adsorption tests

Adsorption isotherms for carbon dioxide were performed applying the volumetric method. This method is fundamentally based on pressure variation of the relevant gas after an expansion. By the knowledge of pressure decrease and assuming ideal gas behaviour for the system, it is possible to determine the concentration of adsorbed solute. Composite membranes were prepared based on polymeric ionic liquids (PILs) with chemically compatible ionic liquids (ILs). One of the composites is made of PIL1 and 40% of ionic liquid (PIL1-40IL1) and the other is made of PIL2 and 20% of ionic liquid (PIL2-20IL2).

- Permeation experiments

Tubular ceramic supports preparation

The preparation of tubular ceramic supports included firstly the blending of porous ends of Al₂O₃ to nonporous Al₂O₃ tubes through a sealing with glass sealant at 1150 °C. The supports have a mean pore size of 200 nm (located in the outer part of the tube), an external diameter of 10 mm and a length of 70 mm. An effective length of approximately 50 mm was left for dip-coating. After this procedure, the membranes were dip coated with yttrium zirconia stabilized (YSZ) solution using a vacuum pump. The YSZ coated on the membranes was dried in a rotating oven at 40 °C for 4 h. The membranes were then coated with the selective solution and were dried also at 40 °C for 24 h.

Permeation measurement

The permeation tests on the produced supported PIL membranes were performed by probing the target pure gases, namely CO₂ and H₂. The gases in study were introduced in the shell side at 500 – 100 kPa feed pressure (Horiba Stec, model UR7340) and the permeated flow rate at room pressure was determined by one of three flowmeters (Bronkhorst, ranges: 0–10, 0– 100, 0–1000 and 0-10000 mLNmin⁻¹).

2.3 Results and discussion

Figures 1 and 2 show carbon dioxide adsorption equilibrium isotherms for PIL1-40IL1 and PIL2-20IL2. Both composite membranes adsorb carbon dioxide, although the adsorption capacity is reduced. The kinetic parameters for both samples are shown in Table 1. At 0.5 bar and 100 °C and 200 °C the diffusivity of PIL1-40IL1 is very fast and at 1 bar PIL2-20IL2 is also very high. Diffusivities were obtained from the uptake curves for polymers PIL1-40IL1 and PIL2-20IL2 – Table 1.

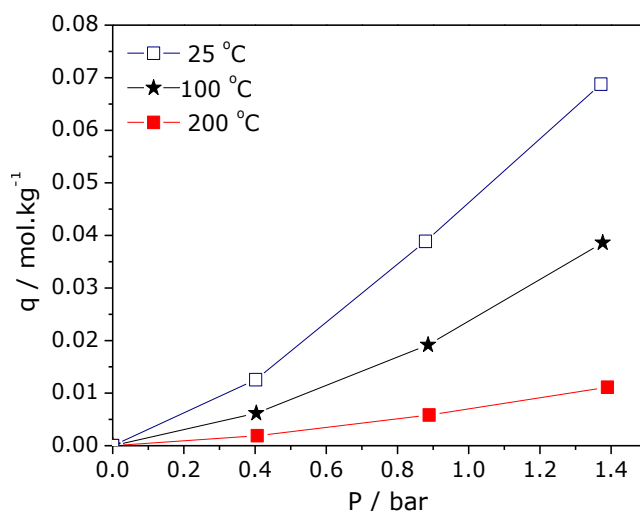


Figure 1 - CO₂ adsorption equilibrium isotherms for PIL1-40IL1 at 25 °C, 100 °C and 200 °C (lines were added for readability).

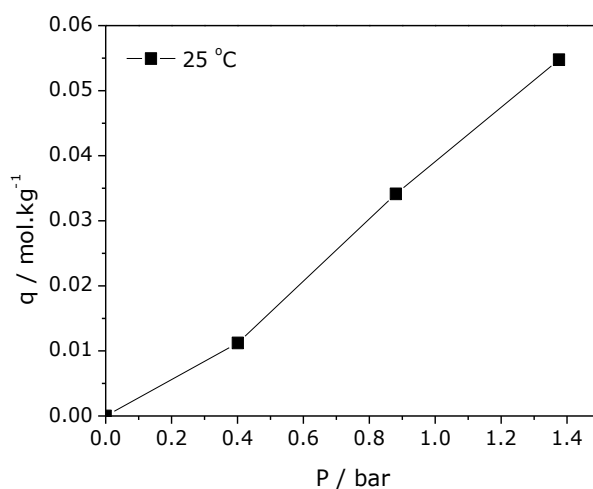


Figure 2 - CO₂ adsorption equilibrium isotherms for PIL2-20IL2 at 25 °C (lines were added for readability).

Table 1 - Kinetic parameters obtained for PIL1-40IL1 and PIL2-20IL2 at 25 °C, 100 °C and 200 °C

Temperature / °C	Sample	Pressure / bar	CO ₂ Diffusivity / s ⁻¹
25	PIL1-40IL1	0.5	2.63×10^{-4}
100			1.73×10^{-3}
200			1.05×10^{-3}
25	PIL2-20IL2	1.0	1.38×10^{-3}

Permeation tests were also performed on polymeric ionic liquid-based membranes in order to obtain pure CO₂ and H₂ permeances. Tables 2, 3 and 3 show the permeances and ideal selectivity as function of feed pressure for PIL1-40IL1, PIL2 (without YSZ calcination) and PIL1 (without YSZ), respectively.

Table 2 - Permeance for PIL1 – 40IL1, at feed pressure of 500 kPa.

Temperature / °C	Permeance / mol.m ⁻² .s ⁻¹ .Pa ⁻¹		Ideal selectivity CO ₂ / H ₂
	CO ₂	H ₂	
25	1.47×10^{-9}	8.89×10^{-11}	> 16.5
50	2.07×10^{-9}	8.89×10^{-11}	> 23.3
100	3.57×10^{-9}	1.35×10^{-9}	2.6
150	5.42×10^{-9}	2.49×10^{-9}	2.2
200	7.62×10^{-9}	4.06×10^{-9}	1.9

Table 3 - Permeance for PIL2 (without YSZ calcination), at feed pressure of 500 kPa.

Temperature / °C	Permeance / mol.m ⁻² .s ⁻¹ .Pa ⁻¹		Ideal selectivity CO ₂ / H ₂
	CO ₂	H ₂	
25	8.89×10^{-11}	5.72×10^{-10}	> 6.4
50	8.89×10^{-11}	5.54×10^{-10}	> 6.2
100	8.89×10^{-11}	1.55×10^{-9}	> 17.5
150	3.21×10^{-8}	1.15×10^{-7}	3.6
200	3.55×10^{-7}	8.51×10^{-8}	4.2

Table 4 - Permeance for PIL1 (without YSZ), at feed pressure of 500 kPa.

Temperature / °C	Permeance / mol.m ⁻² .s ⁻¹ .Pa ⁻¹		Ideal selectivity H ₂ / CO ₂
	CO ₂	H ₂	
25	1.55×10^{-7}	4.28×10^{-7}	2.8
50	1.09×10^{-7}	3.30×10^{-7}	3.0

From Tables 2, 3 and 4 it can be concluded that permeance increases with temperature [3]. It can also be concluded that PIL1-40IL1, PIL1 and PIL2 show facilitated transport due to the heavy presence of amino functional groups, which makes CO₂ to be faster. Polymer membrane 40IL1 shows the best performance. The ideal selectivity decreases abruptly as temperature increases. Low selectivities are then obtained even for low temperatures indicating that the membrane broke. This may happen since the ceramic support has very large pores and does not support properly the polymer membrane.

3. Conclusions

This work characterizes four suitable polymeric ionic liquid-based membranes for low temperature MSR for CO₂ removal. Polymeric ionic liquids were prepared with 40 wt. % and 20 wt. % of free ionic liquid (samples PIL1-40IL1 and PIL2-20IL2) and without free ionic liquid (PIL1 and PIL2). PIL1-40IL1 and PIL2-20IL2 composite membranes present high CO₂ diffusivity and sorption and negligible H₂ diffusivity and sorption. Permeances were also determined for PIL1-40IL1, PIL2 (without YSZ calcination) and PIL1 (without YSZ). Analysing the obtained permeances it was concluded that PIL1-40IL1 shows the highest CO₂/H₂ selectivity. However, PIL1 and PIL2 present higher permeances for H₂ rather than for CO₂. Therefore, it can be presumed that free IL impregnating the polymer membrane enhance the CO₂ permeance.

Task 3.4 was reassessed to respond to the comments and recommendations of the Mid-Term Review of the project (FCH-JU 2014 D2612). Considering that the development and characterization is still undergoing and the limited advances up to M32, no further efforts will be made regarding the task 3.4. This innovative task will be considered in the frame of other projects. The future work will include CO₂ and H₂ permeance measurements for concentrated PIL1/2-40IL1/2 selective solutions dip coated with YSZ solution.

Bibliography

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